EVAPORATORS FOR CHILLING - A REVIEW ON HEAT LOADS, PULLDOWN AND WEIGHT LOSS

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The following section generally discusses industrially accepted methods of chiller design and selecting evaporators for chilling, and compares some results to see how appropriate they are.

Several computer programs were used to help generate data for the discussion. However, these programs have not been used to the ultimate degree, as general data were adequate for this discussion of significant factors.

1. Heat Loads

To calculate the heat load, the industry commonly uses data as illustrated in Tables 1 and 2.

Carcass Weight 205 kg/body (Table 1)

The parameters presented commonly represent chillers designed in the '60s and '70s; carcass weight chosen at 205 kg per body (total weight for 100 bodies = 20,500 kg).

The most significant load in a chiller is the product load, and it is extremely important to have this part correct. The other loads are less significant.

Carcass Weight 350 kg/body (Table 2)

The parameters have been upgraded for product from 205 kg in Table 1 to 350 kg (total weight for 100 bodies = 35,000 kg). Note that the product load has increased dramatically. This illustrates that a chiller designed for 205 kg bodies will generally be inadequate for today's larger bodies.

Type of load		Sensible heat loss (kW)	Latent heat loss (kW)	Total heat loss (kW)	% of total
Conduction - 	Walls Ceiling Floor	1.9 1.8 2.5	-	1.9 1.8 2.5	2.8 2.7 3.7
	Total:	6.3		6.3	9.2
People Lighting Product Motors - - Infiltration	Forklifts Conveyors Fans	0.0 1.1 48.6 0.0 0.0 12.0 0.0	0.0 - - - - 0.0	0.0 1.1 48.6 0.0 0.0 12.0 0.0	0.0 1.6 71.5 0.0 0.0 17.7 0.0
Safety Factor		0.0	0.0	0.0	0.0
Overall Heat Le Heat Loss per C	osses ubic Meter (68.0 W/m ³) - 111.82	0.0 99	68.0	100.0
Input Specifica	tions				
Dimensions (m)	Length Width Height		-	17 6.5 5.5	
Temperatures (° Humidities (%)	C) Ambient Ambient	t/Room t/Room		40°C 30%	1°C 90%
Conduction	Conduction Insulating Material / Conductivity (W/m.K Thickness of Styrene (m) Heat Transfer Coeff. (W/m ² .K) Walls/Floor Ground Temperature (°C) Non-Standard Floor Construction Used				.035 1.200
People Lighting Ventilation	No. of P Lighting No. of A	People in Room 3 Load per Area (Air Changes per 2	0 10 0		
Product	Material to be cooled Initial/Final Temperatures (°C) Heat Capacity (kJ/kg.K) Latent Heat (kJ/kg) Mass in Room (kg) Cooling Time (Hours)			Meat 39 T> -2=3.2 250 20500 12	7 2 T< -2=1.7
Forklifts Conveyors Fans	No. in U No. in U No. in U	Jse * Power Rati Jse * Power Rati Jse * Power Rati	ng/Forklift (W) ng/Conveyor (W) ng/Fan (W)	0 * 0 0 * 0 0 * 0	

0

-0-

Table 1: Heat load for chiller for 100 bodies @ 205 kg

Infiltration

Safety Factor (%)

Type of load		Sensible heat loss (kW)	Laten loss (l	t heat (W)	Total heat loss (kW)	% of total
Conduction - V - C - I	Wall Ceiling Floor	1.9 1.8 2.5	-		1.9 1.8 2.5	1.9 1.8 2.5
- -	Fotal:	6.3	-	-	6.3	6.1
People Lighting Product Motors - I	Forklifts Conveyors	0.0 1.1 83.0 0.0 0.0		0.0 - - -	0.0 1.1 83.0 0.0 0.0	0.0 1.1 81.1 0.0 0.0
- I Infiltration Safety Factor	rans	12.0 0.0 0.0		0.0 0.0	12.0 0.0 0.0	11.7 0.0 0.0
Overall Heat Lo Heat Loss per Cul	sses bic Meter	102.3 (W/m ³) – 168.383	4	0.0	102.3	100.0
Input Specificat	ions					<u> </u>
Dimensions (m)	Length Width Height				17 6.5 5.5	
Temperatures (°C Humidities (%)	C) Ambie Ambie	nt/Room nt/Room			40°C 30%	1°C 90%
Conduction	Insulati Thickn Heat Tr Ground Non-St	ng Material / Conc ess of Styrene (m) ansfer Coeff. (W/m I Temperature (°C andard Floor Con	luctivity () ?.K) Wal) struction 1	W/m.K) ls/Floor Used	Styrene .1 0.338 20°C	.035 1.200
People Lighting Ventilation	No. of Lightir No. of	People in Room g Load per Area (Air Changes per 2	W/m²) 24 hours		0 10 0	
Product	Materia Initial/ Heat C Latent Mass in Cooling	ial to be cooled /Final Temperatures (°C) Capacity (kJ/kg.K) Heat (kJ/kg) in Room (kg) ng Time (Hours)			Meat 39 T>-2=3.2 250 35000 12	7 T<-2=1.7
Forklifts Conveyors Fans Infiltration Safety Factor (%)	No. in No. in No. in	Use * Power Ratin Use * Power Ratin Use * Power Ratin	ng/Forklifi ng/Convey ng/Fan (W	t (W) vor (W) ⁷)	0 * 0 0 * 0 0 * 0 0 0	

Table 2: Heat load for chiller for 100 bodies @ 350 kg

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Carcass Pulldown

What is expected, when one specifies a pulldown from +39°C to 7°C?

What has been calculated, in the heat loads above, is the overall pulldown or the **mass average** pulldown of the total product, **not** the deep-butt.

Is it realistic to pull down deep-butt to $+7^{\circ}$ C in 12 hours? The major factors include body weight and fat cover.

		39°C to 7°C for 400 kg Bodies			
Fig.	0°C Air Temperature	Lean Beef	Heavy Fat		
No.	Air Velocity [m/s]	Hours	Hours		
2.1	0.5	28	36		
2.2	1.0	26	34		
2.3	2.0	25	32		

The above data is generated from Figures 2.1, 2.2 and 2.3. It shows that deep-butt pulldown to 7° C in 12 hours is not practical. It also shows that air velocity has only a small effect on final deep-butt temperature.

However, even withonly 0.5 m/sec air velocity at 0°C air temperature, 350 kg carcasses should comply to EMO250 (to +20°C in 20 hours). To obtain +17°C to +18°C in 16 hours is much more practical. Hence, the mass average carcass temperature is generally +12°C for the 350 kg carcass. Therefore, the assumption in Tables 1 and 2 for the pulldown of 39°C to +7°C in 12 hours is somewhat unrealistic.

The sensible product load for Table 2, should be calculated from 39° C to $+12^{\circ}$ C in 16 hours (52.5 kW in lieu of 83 kW).

Latent Heat from Product

The analysis in Tables 1 and 2 is conservative in sensible heat allowance, however, there is no latent heat allowance. We know this is not possible; there is always some drying of the sides, hence weight loss.

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Considering a weight of 1.3% (hot dry to cold dry) on a total of 35,000 kg of product relates to 455 kg loss weight through the chilling process. Assuming the weight loss is pure water and a chilling duration of 16 hours, the **average product** latent load is approximately 19.7 kW. [This assumption is not strictly correct, the fluid would comprise some salts and organics in small quantities.]

Heat Load Profile

What is commonly calculated for a chiller heat load is the **average summary and cycle load** only. The actual cycle load profile would exceed this load in the first half of the cycle and lessen in the latter half of the cycle as the carcass temperature cools and approaches that of the chiller air temperatures.

A typical load profile for the 350 kg bodies has been presented in Figure 1.



Figure 1: Chilling load profile

unit and generally not depth, as the deeper the coil, the more moisture it removes. In general it is unwise to use 'old' air coolers from general storage facilities for carcass chilling, as it is usually a deep coil.]

A modulating suction pressure regulator is also desirable, to allow the air coolers to always operate at the highest possible suction condition as the heat load drops.

3. Weight Loss

Vapour Pressure

Weight loss can be simply described as the evaporation of the moisture from the wet body surface to the surrounding air.

The potential to lose weight is the difference between the surface water vapour pressure and the partial pressure of the surrounding air. The larger the difference, the larger the potential.

Vapour pressure, in turn, is related to temperature. The larger the difference, the larger the potential. Hence, it is especially important to reduce the surface temperature of the bodies as soon as it is practicable, to minimise weight loss.

Figures 3 and 4, illustrate the difference between designing at the cycle average and above the average. The difference in area between the curves provides an indication of the potential to save weight, which is 30%.



Figure 3: Vapour pressure difference - fast pulldown



Figure 4: Vapour pressure difference - slow pulldown

Air Velocity Consideration

It is important to have good air velocity and air distribution within a chiller, however, equipment layout has not been covered within the scope of this discussion.

With regard to weight loss, there is evidence that the most economical air velocity is between 0.7 to 1.3 m/sec for carcass weight between 250 to 350 kg. Furthermore, there is almost no real change in evaporative weight loss with increasing air velocity over the above values. The main reason for this is the balance between heat transfer and mass transfer. The two are inter-related, that is:

1. The higher the velocity, the higher the heat transfer, hence quicker pulldowns, lower vapour pressure difference, a lower weight loss potential on one hand,

but,

2. The higher the air velocity, the higher the potential for mass transfer (evaporation), hence a higher potential to lose weight on the other hand.

The latter is less significant with velocity less than 1.5 m/sec and good air temperature, generally of 0°C (Figure 6 shows the typical relationship described above).



Figure 5: Deep leg temperature



Figure 6: Weight loss versus air velocity

4. Conclusion

The main conclusion, without going into detail, can be put simply, as:

The more "appropriate" the surface area (capacity), the higher the product quality and lower the weight loss.

However, finding the "balance" which is economical and suits your requirements is also important. Hence, knowing specifically what the realistic goals are, and knowing what factors are significant, will assist.

5. References

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